# A new diffusive model for rarefied gas dynamics 

Julien Mathiaud (CEA/CESTA), Luc Mieussens (IMB)

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1 Context and models

2 The ES Fokker Planck model

3 Chapman Enskog expansion and final model

4 Numerical results

5 Conclusion \& Perspectives

## Context and objectives



## Objectives

- Capture the correct thermal fluxes in order to design re-entry vehicles,
- Use a kinetic model able to recover Navier-Stokes equations in its hydrodynamic limit to ensure a continuity in models.
- One key point is to recover the correct Prandtl number:

$$
\operatorname{Pr}=\frac{\gamma R}{\gamma-1} \frac{\mu}{\kappa}
$$

(equal to $\frac{2}{3}$ for monoatomic gases) .

## cea Zoology of models (1): Boltzmann equation

$$
\begin{equation*}
\partial_{t} f+v \cdot \nabla_{x} f=Q(f, f) \tag{1}
\end{equation*}
$$

with

$$
Q(f, f)(v)=\int_{v_{*} \in \mathbb{R}^{3}} \int_{\sigma \in S^{2}}\left(f\left(v_{*}^{\prime}\right) f\left(v^{\prime}\right)-f\left(v_{*}\right) f(v)\right) r^{2}\left|v-v_{*}\right| d \sigma d v_{*}
$$

and

$$
\begin{aligned}
& v^{\prime}=\frac{v+v_{*}}{2}+\frac{\left|v-v_{*}\right|}{2} \sigma \\
& v_{*}^{\prime}=\frac{v+v_{*}}{2}-\frac{\left|v-v_{*}\right|}{2} \sigma
\end{aligned}
$$

## Advantages and drawbacks

+ Capture the correct physics: in the Chapman expansion one recovers the Prandtl number of Navier-Stokes equation which is equal to $\frac{2}{3}$
- High numerical cost in transitional area between 100km and 60km (6D non linear problem).


## Fokker Planck equation

## BGK equation

$$
\begin{equation*}
\partial_{t} f+v \cdot \nabla_{x} f=\frac{1}{\tau}(M(f)-f) \tag{2}
\end{equation*}
$$

$M(f)=\frac{\rho}{(2 \pi R T)^{3 / 2}} \exp \left(\frac{|v-u|^{2}}{2 R T}\right)$ is the Maxwellian of equilibrium satisfying:
$<f>=\int f d v=\rho,<f v>=\int f v d v=\rho u,<f \frac{1}{2}(v-u)^{2}>=\int f \frac{1}{2}(v-u)^{2} d v=\frac{3}{2} \rho T$
$\tau$ : characteristic time of collisions.
Fokker Planck equation

$$
\begin{equation*}
\partial_{t} f+v \cdot \nabla_{x} f=\frac{1}{\tau} \nabla_{v} \cdot\left((v-u) f+T \nabla_{v} f\right) \tag{3}
\end{equation*}
$$

## Advantages and drawbacks

- Physics only approximated: thermal flux underestimated. The Prandtl number is equal to 1 for BGK model and $\frac{3}{2}$ for $F P$ model.
+ Numerical cost less important in transitional area between 100km and 60km.


## How to recover the correct Prandtl number?

For BGK models it has been done using the ESBGK model:

$$
\begin{equation*}
\partial_{t} f+v \cdot \nabla_{x} f=\frac{1}{\tau}(G(f)-f) \tag{4}
\end{equation*}
$$

with $G(f)$ anisotropic Gaussian defined as
$G(f)=\frac{\rho}{\sqrt{\operatorname{det}(2 \pi \Pi)}} \exp \left(-\frac{(v-u) \Pi^{-1}(v-u)}{2}\right)$.
$\Pi$ being a tensor linked to the different temperatures of thermal agitation.

## Cea Equation of the ESFP model (1)

The model is the following:

$$
\begin{equation*}
\partial_{t} f+v \cdot \nabla_{x} f=D(f), \tag{5}
\end{equation*}
$$

where the collision operator is defined by

$$
\begin{equation*}
D(f)=\frac{1}{\tau} \nabla_{v} \cdot\left((v-u) f+\Pi \nabla_{v} f\right) \tag{6}
\end{equation*}
$$

where $\tau$ is a relaxation time, and $\Pi$ is a convex combination between the temperature tensor $\Theta$ and its equilibrium value RTI, that is to say:

$$
\begin{equation*}
\Pi=(1-\nu) R T I+\nu \Theta, \tag{7}
\end{equation*}
$$

with $\nu$ parameter to be set and

$$
\begin{equation*}
\Theta:=\frac{1}{\rho}\langle(v-u) \otimes(v-u) f\rangle . \tag{8}
\end{equation*}
$$

## cea Other formulations for ESFP

The operator $D$ has two other equivalent formulations:

$$
\begin{equation*}
D(f)=\frac{1}{\tau} \nabla_{v} \cdot\left(\Pi G(f) \nabla_{v} \frac{f}{G(f)}\right), \tag{9}
\end{equation*}
$$

and

$$
\begin{equation*}
D(f)=\frac{1}{\tau} \nabla_{v} \cdot\left(\Pi f \nabla_{v} \log \left(\frac{f}{G(f)}\right)\right) \tag{10}
\end{equation*}
$$

where $G(f)$ is the anisotropic Gaussian defined by

$$
\begin{equation*}
G(f)=\frac{\rho}{\sqrt{\operatorname{det}(2 \pi \Pi)}} \exp \left(-\frac{(v-u) \Pi^{-1}(v-u)}{2}\right) \tag{11}
\end{equation*}
$$

which has the same 5 first moments as $f$

$$
\left\langle\left(1, v, \frac{1}{2}|v|^{2}\right) G(f)\right\rangle=(\rho, \rho u, E),
$$

and has the temperature tensor $\langle(v-u) \otimes(v-u) G(f)\rangle=\Pi$.

## Condition of strict positiveness of $\Pi$

The tensor $\Pi$ is symmetric positive definite for every tensor $\Theta$ if, and only if,

$$
\begin{equation*}
-\frac{R T}{\lambda_{\max }-R T}<\nu<\frac{R T}{R T-\lambda_{\min }}, \tag{12}
\end{equation*}
$$

where $\lambda_{\max }$ and $\lambda_{\text {min }}$ are the (positive) maximum and minimum eigenvalues of $\Theta$.
Moreover $\Pi$ is unconditionally definite positive with respect to the eigenvalues of $\Theta$ as long as :

$$
\begin{equation*}
-\frac{1}{2}<\nu<1 . \tag{13}
\end{equation*}
$$

## cea Kinetic properties of the model:

## Conservation

We suppose that the condition of strict positiveness (equations 12) is fulfilled by $\nu$. The operator $D$ conserves the mass, momentum, and energy:

$$
\left\langle\left(1, v, \frac{1}{2}|v|^{2}\right) D(f)\right\rangle=0 .
$$

## Entropy decay

$$
\langle D(f) \log f\rangle \leq 0
$$

## Equilibrium

$$
D(f)=0 \Leftrightarrow f=G(f) \Leftrightarrow f=M(f) .
$$

## cea Chapman Enskog expansion

## Non dimensional ESFP equation

Assume we have some reference values of length $x$, pressure $p$, and temperature $T$.
We can derive reference values for all the other quantities: mass density $\rho=p / R T$, velocity $v=\sqrt{R T}$, time $t_{*}=x / v$, distribution function $f=\rho /(R T)^{3 / 2}$. We also assume we have a reference value for the relaxation time $\tau$.

$$
\begin{equation*}
\partial_{t} f+v \cdot \nabla_{x} f=\frac{1}{\varepsilon} D(f) \tag{14}
\end{equation*}
$$

where $\varepsilon=\frac{v \tau}{x}$ is the Knudsen number.

The solution of the ESFP model satisfies, up to $O\left(\varepsilon^{2}\right)$ the Navier-Stokes equations ( $\varepsilon$ being the Knudsen number defined below):

$$
\begin{align*}
& \partial_{t} \rho+\nabla \cdot \rho u=0, \\
& \partial_{t} \rho u+\nabla \cdot(\rho u \otimes u)+\nabla p=-\nabla \cdot \sigma,  \tag{15}\\
& \partial_{t} E+\nabla \cdot(E+p) u=-\nabla \cdot q-\nabla \cdot(\sigma u),
\end{align*}
$$

where the shear stress tensor and the heat flux are given by

$$
\begin{equation*}
\sigma=-\mu\left(\nabla u+(\nabla u)^{T}-\frac{2}{3} \nabla \cdot u\right), \quad \text { and } \quad q=-\kappa \nabla \cdot T, \tag{16}
\end{equation*}
$$

The viscosity and heat transfer coefficients are following:

$$
\begin{equation*}
\mu=\frac{\tau p}{2(1-\nu)}, \quad \text { and } \quad \kappa=\frac{5}{6} \tau p R . \tag{17}
\end{equation*}
$$

The corresponding Prandtl number is $\operatorname{Pr}=\frac{3}{2(1-\nu)}$.

## cea Complete ESFP model

## Pros and cons

- We can only recover a Prandtl of 1 because $\nu$ is bounded below by $-\frac{1}{2}$ to ensure positiveness of the $\Theta$ tensor.
+ In real cases near equilibrium $\Theta$ is nearly equal to TId so that we can use $\nu=-\frac{5}{4}$ and recover the correct Prandtl number.


## Complete ESFP model

$$
\begin{aligned}
& \partial_{t} f+v \cdot \nabla_{x} f=D(f), \\
& D(f)=\frac{1}{\tau} \nabla_{v} \cdot\left((v-u) f+\Pi \nabla_{v} f\right), \\
& \Pi=\left(1-\nu_{\text {eff }}\right) R T I+\nu_{\text {eff }} \Theta, \\
& \left.\nu_{\text {eff }}=\max \left(-\frac{5}{4},-\frac{R T}{\lambda_{\max }-R T}\right)\right) .
\end{aligned}
$$

## Cea Numerical method

## Solving the collision operator

We use standard DSMC methods to proceed. Re-normalization is used to provide noiseless moments of the p.d.f. . One million particles are used.

## Numerical test cases and solutions

- We present only 0-D test cases,
- Validation is made through two test cases, one with inactive correction on $\nu$ and one with active correction,
- One should recover the following ODEs for the $\Theta$ tensor and the third moment $q$.

$$
\begin{aligned}
& \frac{d}{d t} \Theta=\frac{1}{\tau} 2(1-\nu)(R T-\Theta) \\
& \Theta(t)=\exp \left(-\frac{2(1-\nu) t}{\tau}\right) \Theta(0)+\left(1-\exp \left(-\frac{2(1-\nu) t}{\tau}\right)\right) R T I, \\
& \text { (for } \nu \text { constant) } \\
& \frac{d}{d t} q=-\frac{3}{\tau} q, \text { so that } q(t)=q(0) \exp \left(-\frac{3 t}{\tau}\right) .
\end{aligned}
$$

Numerical results for an homogeneous case: $\partial_{t} f=D(f)$ with inactive correction



- On the left: behaviour of the diagonal components $T_{11}, T_{22}, T_{33}$ of tensor $\Theta$ and of its trace $T$.
- On the right: histogram of the first component of velocity at time $t=1$.

Numerical results for an homogeneous case: $\partial_{t} f=D(f)$ with inactive correction



- On the left: $\nu$ and $\operatorname{Pr}$ along time.
- On the right: convergence of the logarithms of $\left|T-T_{11}\right|$ and $q$
- the Prandtl number numerically captured is equal to
$P r_{n}=\frac{2.8971}{4.5001}=0.6428$

- On the left: behaviour of the diagonal components $T_{11}, T_{22}, T_{33}$ of tensor $\Theta$ and of its trace $T$.
- On the right: histogram of the first component of velocity at time $t=0.5$.


##  Numerical results for an homogeneous case: $\partial_{t} f=D(f)$ with active correction



- On the left: $\nu$ and $\operatorname{Pr}$ along time.
- On the right: convergence of the logarithms of $\left|T-T_{11}\right|$ and $q$


## COZ Numerical results for an homogeneous case: $\partial_{t} f=D(f)$ with active correction



- On the left: comparison between $\log \left(\left|T-T_{11}\right|\right)$ ant its linear fitting.
- On the right: comparison between $\log (|q|)$ ant its linear fitting.


## cea Conclusion \& Perspectives

- Construction of a new kinetic model able to recover the correct Prandtl number in the hydrodynamic limit,
- More numerical tests need to be performed with a non homogeneous code,
- Extension to polyatomic gases necessary for real cases,
- Extension to chemistry / sprays should be investigated.

- Convergence towards equilibrium for the different temperatures

